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WINGBOX



Validation V1



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Validation from known cases

The following cases are a subset of many cases that were used to validate WINGBOX. The ones presented here are taken from the book of T.H.G. MEGSON.

Some small differences might exist between the results given by MEGSON and they are due to some modelling approximations done, or number of decimals used in the hand-calculations of the book.


```

COORDINATES OF NODE   5 :   1246.000000   -152.000000   0.000000
COORDINATES OF NODE   6 :   1754.000000   -102.000000   0.000000
COORDINATES OF NODE   7 :         0.000000         0.000000   0.000000

```

```

WX=  0.000000E+00   WY=  0.000000E+00
SX=  0.000000E+00   SY=  0.100000E+01
BMX= 0.000000E+00   BMY=  0.000000E+00

```

X DISTANCE OF SY FORCE APPLICATION: 484.0000

```

CENTROID :   949.666667   0.000000   0.000000

```

```

SECTIONAL-AREA=  7740.000000

```

Second moments about Centroid:

```

IXX=  0.162442E+09   IYY=  0.190032E+10   IXY= -0.745058E-08
I11=  0.162442E+09   I22=  0.190032E+10   I12= -0.745058E-08   I33=  0.206276E+10

```

```

NEUTRAL AXIS INCLINATION :   0.00 DEGREES

```

```

SHEAR CENTRE COORDINATES=       731.5441       -0.0000       0.0000

```

SHEAR CENTER

```

I11=  0.162442E+09   I22=  0.226857E+10   I12=  0.119209E-06   I33=  0.243101E+10

```

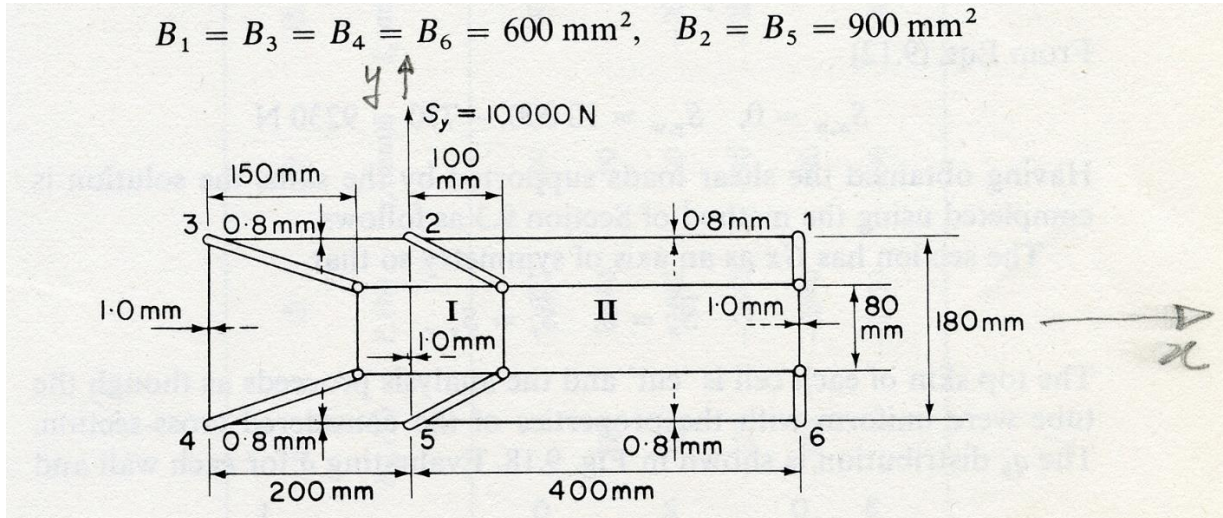
Since the spar 34 is at a distance 484mm then the Shear Centre location is

$$731.5 - 484 = 247.5\text{mm}$$

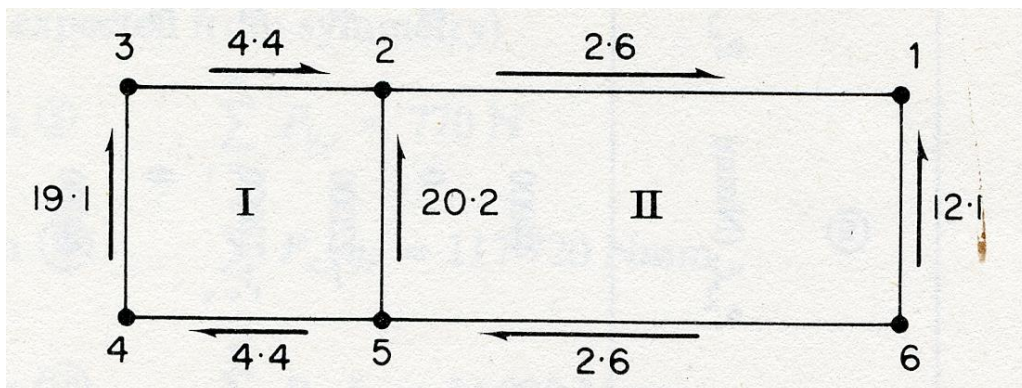
The quoted value was **240mm**, the difference with WINGBOX is due to the approximation of the shape of the Cell I, which appears parabolic in the definition while it was modelled as triangular (of the same length 1015mm) for the sake of simplicity for this exercise.

Multicell example for the validation of the Taper

The following tapered section was loaded by a Shear Force as on the diagram and a Bending Moment of -1650000 Nmm. The length of the tapered multicell was 1200mm.



The shear flows on the larger section where to be found. The reference answer is as below:



Analysing it with WINGBOX and assuming a counterclockwise positive shear flow convention, the following was obtained for the larger section:

COORDINATES OF NODE	1 :	600.000000	90.000000	0.000000
		600.000000	40.000000	1200.000000
COORDINATES OF NODE	2 :	200.000000	90.000000	0.000000
		300.000000	40.000000	1200.000000
COORDINATES OF NODE	3 :	0.000000	90.000000	0.000000
		150.000000	40.000000	1200.000000
COORDINATES OF NODE	4 :	0.000000	-90.000000	0.000000
		150.000000	-40.000000	1200.000000
COORDINATES OF NODE	5 :	200.000000	-90.000000	0.000000
		300.000000	-40.000000	1200.000000
COORDINATES OF NODE	6 :	600.000000	-90.000000	0.000000
		600.000000	-40.000000	1200.000000

WX= 0.000000E+00 WY= 0.000000E+00
 SX= 0.000000E+00 SY= 0.100000E+05
 BMX= -0.165000E+07 BMY= 0.000000E+00

SXBAR-taper= -0.568434E-13 SYBAR-taper= 0.923611E+04

CENTROID : 257.142857 0.000000 0.000000

SECTIONAL-AREA= 4200.000000

IXX= 0.340200E+08 IYY= 0.226286E+09 IXY= 0.000000E+00
 I11= 0.340200E+08 I22= 0.226286E+09 I12= 0.000000E+00 I33= 0.260306E+09

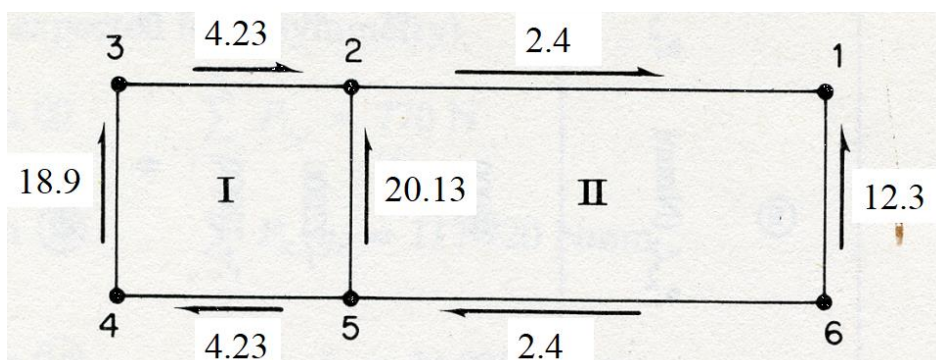
SHEAR CENTRE COORDINATES= 258.7709 0.0000 0.0000

SHEAR CENTER

I11= 0.340200E+08 I22= 0.226297E+09 I12= 0.000000E+00 I33= 0.260317E+09

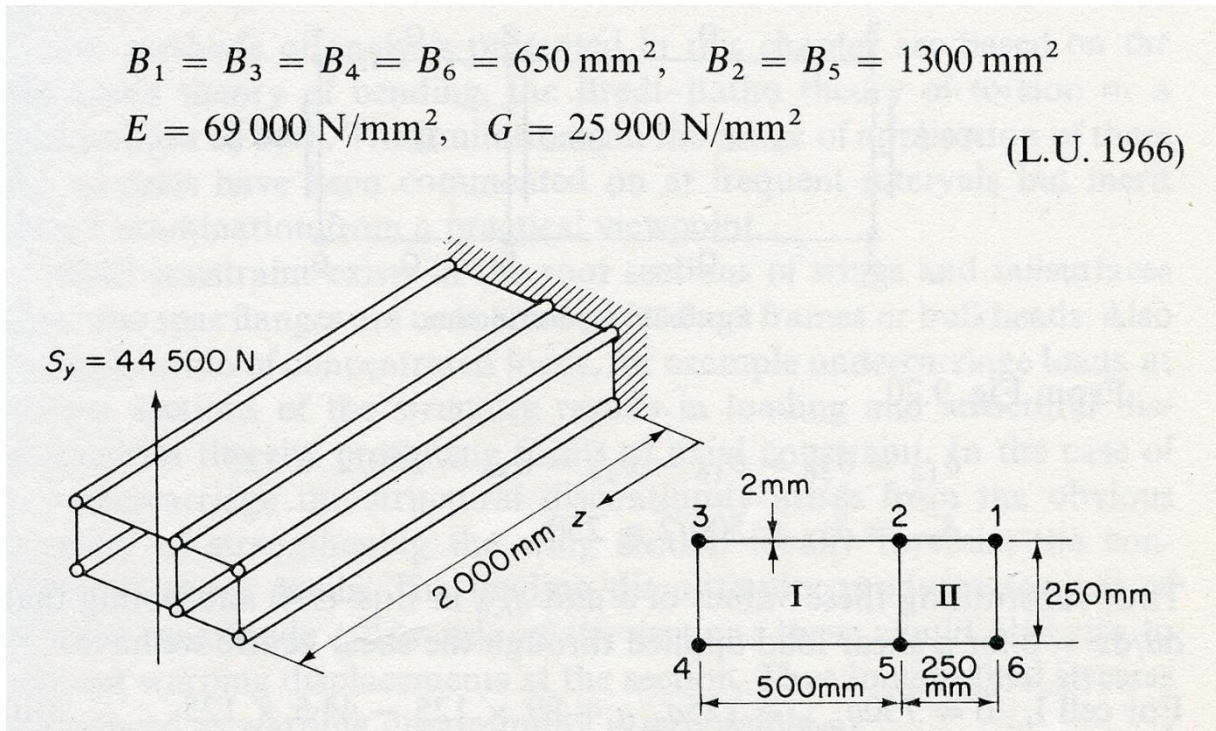
SHEAR FLOW for Cell: 1	NODAL SEGMENT:	2	3			
VALUES:		-4.228287	-4.228287	-4.228287	-4.228287	-4.228287
SHEAR FLOW for Cell: 1	NODAL SEGMENT:	3	4			
VALUES:		-18.888781	-18.888781	-18.888781	-18.888781	-18.888781
SHEAR FLOW for Cell: 1	NODAL SEGMENT:	4	5			
VALUES:		-4.228287	-4.228287	-4.228287	-4.228287	-4.228287
SHEAR FLOW for Cell: 1	NODAL SEGMENT:	5	2			
VALUES:		20.131879	20.131879	20.131879	20.131879	20.131879
SHEAR FLOW for Cell: 2	NODAL SEGMENT:	1	2			
VALUES:		-2.369425	-2.369425	-2.369425	-2.369425	-2.369425
SHEAR FLOW for Cell: 2	NODAL SEGMENT:	2	5			
VALUES:		-20.131879	-20.131879	-20.131879	-20.131879	-20.131879
SHEAR FLOW for Cell: 2	NODAL SEGMENT:	5	6			
VALUES:		-2.369425	-2.369425	-2.369425	-2.369425	-2.369425
SHEAR FLOW for Cell: 2	NODAL SEGMENT:	6	1			
VALUES:		12.291068	12.291068	12.291068	12.291068	12.291068

which gives pictorially :



Multicell example for the validation of the Displacements

The following section was loaded by a Shear Force as on the diagram passing from the Shear Center. The length of the multicell was 2000mm.



The vertical displacement due to the shear force was referenced to be:

$$\Delta = 23.5 \text{ mm.}$$

Analysing it with WINGBOX and assuming a counterclockwise positive shear flow convention, the following was obtained for the section:

First an analysis was done with a fictitious location of the application of the vertical shear force just to get WINGBOX to calculate the Shear Center. This was found to be :

SHEAR CENTRE COORDINATES= 432.0652 125.0000 0.0000

Then the above location was used as the application point of the shear force and the following was obtained:

COORDINATES OF NODE	1 :	750.000000	250.000000	0.000000
		750.000000	250.000000	2000.000000
COORDINATES OF NODE	2 :	500.000000	250.000000	0.000000
		500.000000	250.000000	2000.000000
COORDINATES OF NODE	3 :	0.000000	250.000000	0.000000


```

                                0.000000    250.000000    2000.000000
COORDINATES OF NODE    4 :    0.000000    0.000000    0.000000
                                0.000000    0.000000    2000.000000
COORDINATES OF NODE    5 :    500.000000    0.000000    0.000000
                                500.000000    0.000000    2000.000000
COORDINATES OF NODE    6 :    750.000000    0.000000    0.000000
                                750.000000    0.000000    2000.000000

```

```

WX= 0.000000E+00    WY= 0.000000E+00
SX= 0.000000E+00    SY= 0.445000E+05
BMX= 0.000000E+00    BMY= 0.000000E+00

```

X DISTANCE OF SY FORCE APPLICATION: 432.0652

```

CENTROID :    437.500000    125.000000    0.000000

```

```

SECTIONAL-AREA=    5200.000000

```

```

IXX= 0.812500E+08    IYY= 0.385938E+09    IXY= 0.000000E+00
I11= 0.812500E+08    I22= 0.385938E+09    I12= 0.000000E+00    I33= 0.467188E+09

```

```

WXBAR= 0.000000E+00    WYBAR= 0.000000E+00
SXBAR= 0.000000E+00    SYBAR= 0.445000E+05
BMXBAR= 0.000000E+00    BMYBAR= 0.000000E+00

```

```

SXBAR-taper= 0.000000E+00    SYBAR-taper= 0.445000E+05

```

```

NEUTRAL AXIS INCLINATION :    0.00 DEGREES

```

```

SHEAR CENTRE COORDINATES=    432.0652    125.0000    0.0000

```

SHEAR CENTER

```

I11= 0.812500E+08    I22= 0.386091E+09    I12= -0.372529E-08    I33= 0.467341E+09

```

```

X-DISPLACEMENT:    -0.00000    -0.00000    -0.00000    -0.00000    -0.00000
Y-DISPLACEMENT:    23.59890    16.84710    10.60331    5.37553    1.67175
X-ROTATION:    -0.91004    -0.87364    -0.76443    -0.58243    -0.32761
Y-ROTATION:    0.00000    0.00000    0.00000    0.00000    0.00000
Z-ROTATION:    -0.00000    -0.00000    -0.00000    -0.00000    -0.00000

```

The above displacement and rotation (in degrees) results correspond to the distributions along the flexural axis of the multicell, from the tip to the “encastre” end. Five segments were assigned for the distribution definition.

It can be seen that the maximum vertical displacement (along the flexural axis of the beam) is **23.5989 mm** as compared to **23.5mm reference**.

Also the shear flow distribution was found as:

SHEAR FLOW for Cell: 1	NODAL SEGMENT: 2	3			
VALUES: -5.804350	-5.804350	-5.804350	-5.804350	-5.804350	-5.804350
SHEAR FLOW for Cell: 1	NODAL SEGMENT: 3	4			
VALUES: -50.304350	-50.304350	-50.304350	-50.304350	-50.304350	-50.304350
SHEAR FLOW for Cell: 1	NODAL SEGMENT: 4	5			
VALUES: -5.804350	-5.804350	-5.804350	-5.804350	-5.804350	-5.804350
SHEAR FLOW for Cell: 1	NODAL SEGMENT: 5	2			
VALUES: 73.521739	73.521739	73.521739	73.521739	73.521739	73.521739
SHEAR FLOW for Cell: 2	NODAL SEGMENT: 1	2			
VALUES: 9.673911	9.673911	9.673911	9.673911	9.673911	9.673911
SHEAR FLOW for Cell: 2	NODAL SEGMENT: 2	5			
VALUES: -73.521739	-73.521739	-73.521739	-73.521739	-73.521739	-73.521739
SHEAR FLOW for Cell: 2	NODAL SEGMENT: 5	6			
VALUES: 9.673911	9.673911	9.673911	9.673911	9.673911	9.673911
SHEAR FLOW for Cell: 2	NODAL SEGMENT: 6	1			
VALUES: 54.173911	54.173911	54.173911	54.173911	54.173911	54.173911

while the reference values were:

$$\begin{aligned}
 q_{0,12} &= 9.6 \text{ N/mm}, & q_{0,23} &= -5.8 \text{ N/mm}, & q_{0,43} &= 50.3 \text{ N/mm}, \\
 q_{0,45} &= -5.8 \text{ N/mm}, & q_{0,56} &= 9.6 \text{ N/mm}, & q_{0,61} &= 54.1 \text{ N/mm}, \\
 q_{0,52} &= 73.6 \text{ N/mm}
 \end{aligned}$$